#### **REMARKS ON SOME PROPERTIES OF THE EQUATION OF** TRANSFER IN HEAT MULTICHANNEL EXCHANGERS

# T. ZALESKI and A. B. JARZEBSKI

Polish Academy of Sciences, Research Centre of Chemical Engineering and Chemical Apparatus Construction, Gliwice, Poland

(Received 30 August 1972 and in revised form 12 December 1972)

Abstract—Some properties of the equation of heat transfer in n-channel mixed parallel and counter-flow exchangers are discussed. It is shown that the matrix of coefficients A is of rank n-1, and the necessary and sufficient condition for A to have two zero latent roots is given.

#### NOMENCLATURE

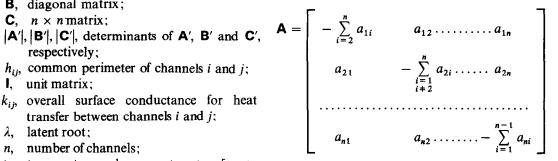
- $a_{ii}$ , number of transfer units per unit of coordinate x:  $a_{ij} = k_{ij}h_{ij}/W_i$ ;
- **A**, coefficient matrix;
- **A'**, **B'**, **C'**, matrices of order n-1;
- **B**, diagonal matrix;

- *n*, number of channels:
- t. temperature column vector,  $\mathbf{t} = [t_1, t_2, t_3]$  $\ldots t_n$ <sup>T</sup>
- $t_i$ , temperature of fluid in channel *i*;
- W, fluid heat capacity rate;
- x, space coordinate along the channel.

THE theoretical analysis of the temperature distribution in the fluids in multichannel mixed parallel and counter-flow heat exchangers, for steady state heat transfer, is described with sufficient accuracy, by a system of linear ordinary differential equations with constant coefficients

$$\frac{\mathrm{d}t}{\mathrm{d}x} = \mathbf{A}t \tag{1}$$

where t is the column matrix of temperatures and A is a square matrix of order n



Wolf presents the general solution of system (1) assuming that multiple zero latent roots of A cannot exist [1]. He proves that all the latent roots are distinct with the same assumption. Settari proves that all the latent roots are real [2]; whilst not negating Wolf's theorem concerning distinct non-zero latent roots, he shows that two zero latent roots can exist, giving a plate exchanger consisting of four channels connected in series (Fig. 1) as an example.

It may be noted that multiple zero latent roots may exist in other types of exchangers as well [3-6].

An analysis of Settari's paper has led us to the following conclusions.

I. The existence of two zero latent roots leads Settari to conclude that **A** may be doubly degenerate, probably because of an incorrect

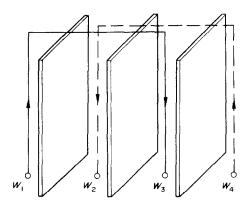


FIG. 1. Typical plate exchanger geometry.

interpretation of a theorem given by Hildebrand [7]. As we shall see later, this would imply a particular geometry and structure of an exchanger.

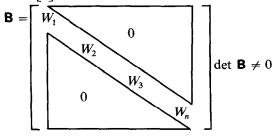
We shall now prove

# Theorem 1

If A is not a diagonal block matrix, the rank of A is always equal to n - 1.

## Proof

As in [2], let us introduce matrices



and



where 
$$c_{ij} = h_{ij}k_{ij} = c_{ji}$$
 for  $i \neq j$   
 $c_{ii} = -\sum_{ij}^{n} h_{ij}k_{ij}$  and  $k_{ij}h_{ij} = 0$ 

can be represented by the product

$$\mathbf{C} = \mathbf{B}\mathbf{A}.\tag{2}$$

Striking out the last row and column of A, B and C we obtain matrices A', B' and C' respectively, of order n - 1. Clearly

$$\mathbf{C}' = \mathbf{B}'\mathbf{A}'. \tag{3}$$

As **C'** is symmetric it must be irreducible. It is also diagonally dominant with strict inequality for  $c_{n-1, n-1}$ , then **C'** is an irreducibly diagonal dominant matrix. Hence from theorem 1.8 ([8] p. 23) we conclude that **C'** is non-singular and  $|\mathbf{C'}| = |\mathbf{B'}||\mathbf{A'}|$  then **A'** is non-singular and  $|\mathbf{A'}|$  does not vanish completing the proof.

Diagonal block matrices are excluded from consideration because any such matrix represent two or more thermally isolated sub-exchangers.

II. The possibility of multiple zero latent roots is determined by

# Theorem 2

The necessary and sufficient condition for A to have two zero latent roots is that the sum of diagonal elements of **B** is zero.

# Proof

We first prove the following lemma

All the cofactors of **C** are equal.

*Proof.* Let us consider the cofactors of  $c_{ni}$  and  $c_{n,i+1}$ , denoted by  $C_{ni}$  and  $C_{n,i+1}$  respectively

$$C_{ni} = (-1)^{n+i} \begin{vmatrix} c_{11} c_{12} \dots c_{1,i-1} c_{1,i+1} \\ c_{1,i+2} \dots c_{1n} \\ c_{21} c_{22} \dots c_{2,i-1} c_{2,i+1} \\ c_{2,i+2} \dots c_{2n} \\ \dots \\ c_{n-1,1} c_{n-1,2} \dots c_{n-1,i-1} \\ c_{n-1i+1} c_{n-1,1+2} \dots c_{n-1,n} \end{vmatrix}$$

$$C_{n,i+1} = (-1)^{n+i+1} \begin{vmatrix} c_{11} c_{12} \dots c_{1,i-1} c_{1i} \\ c_{1,1+2} \dots c_{1n} \\ c_{2i} c_{2i} \dots c_{2i-1} c_{2i} \\ c_{2,i+2} \dots \dots c_{2n} \\ \dots \\ c_{n-1,1} c_{n-1,2} \dots c_{n-1,i-1} \\ c_{n-1,i} c_{n-1,i-1} - c_{n-1,i-1} \\ c_{n-1,i} c_{n-1,i-1} - c_{n-1,i-1} \end{vmatrix}$$

The properties of  $\mathbf{C}$  show that  $C_{ni}$  is obtained when we add all the other columns to column *i* of  $C_{n,i+1}$ . Hence all the cofactors of the entries of the bottom row of  $\mathbf{C}$  are equal. The same method can be used to prove that the cofactors of an arbitrary *i*-th row are all equal. If they are denoted by  $C_i$  the cofactors of the column *n* are  $C_1, C_2, \ldots, C_n$  respectively, but as  $\mathbf{C}$  is symmetric, they must be equal to those of the *n*-th row, thus

$$C_1 = C_2 = \ldots = C_n = C_A$$

completing the proof of the lemma.

Theorem 1 shows that  $C_A \neq 0$ 

From (2) we may write

B

$$\mathbf{A} = \mathbf{B}^{-1}\mathbf{C}. \tag{4}$$

Let  $B_1^{-1}, B_2^{-1}, \ldots, B_n^{-1}$  be the cofactors of the diagonal elements of  $\mathbf{B}^{-1}$ .

The sum of first principal minors of A is then

$$(B_1^{-1} + B_2^{-1} + \ldots + B_n^{-1}) C_A$$

but as it is the coefficient of the linear term of the characteristic equation  $|\mathbf{A} - \mathbf{i}\lambda| = 0$ , the neces-

sary and sufficient condition for A to have two zero latent roots is

$$B_1^{-1} + B_2^{-1} + \dots + B_n^{-1} = \frac{\sum_{i=1}^{n} W_i}{\prod_{i=1}^{n} W_i} = 0 \qquad (5)$$

hence

$$\sum_{i=1}^{n} W_i = 0$$

which had to be proved.

III. The heat exchanger considered by Settari ([2], Fig. 1) and shown in Fig. 1 of this communication always fulfils the conditions of theorem 2 as  $W_3 = -W_1$  and  $W_2 = -W_4$ . Therefore, the matrix **A** arising from this heat exchange system possesses two zero latent roots irrespective of the direction of flow in the two circuits. This result differs from that of Settari [2] who concludes that the number of zero latent roots is one or two, depending on whether or not the flows are in the same direction.

It has been shown [9]. that for plate heat exchangers with number of channels divisible by four, and channels connected as in Fig. 1, the matrix has two and only two zero latent roots. This is, of course, in accordance with theorem 2.

#### REFERENCES

- 1. J. WOLF. General solution of the equations of parallel flow multichannel heat exchangers, *Int. J. Heat Mass Transfer* 7, 901–919 (1964).
- A. SETTARI, Remarks about 'General solution of the equations of multichannel heat exchangers', Int. J. Heat Mass Transfer 15, 555-557 (1972).
- 3. D. D. AULDS and R. F. BARRON, Three fluid heat exchanger effectiveness, Int. J. Heat Mass Transfer 10, 1457-1462 (1967).
- W. OKOŁO KUŁAK, Three agent heat exchangers, Zesz. Nauk. Politech. Slask. Mechanika Nr 1 (1954) (in Polish).
- K. F. FISHER, Mean temperature difference correction in multipass exchangers, *Ind. Engng Chem.* 30 (4), 377-383 (1938).

- 6. T. ZALESKI and W. KRAJEWSKI, Calculation of a screw type heat exchanger, *Inz. Chem.*, in press (in Polish).
- 7. F. B. HILDEBRAND, Methods of Applied Mathematics, 2nd ed. Prentice-Hall, New Jersey (1965).
- 8. R. S. VARGA, *Matrix Iterative Analysis*. Prentice-Hall, New Jersey (1962).
- 9. T. ZALESKI and J. JARZABEK, Calculation of a plate exchanger with channels connected in series, *Inz. Chem.* in press (in Polish).

### REMARQUES SUR QUELQUES PROPRIETES DE L'EQUATION DE TRANSFERT THERMIQUE DANS DES ECHANGEURS MULTI-CANAUX

**Résumé**—On discute quelques propriétés de l'équation de transfert thermique dans des échangeurs à n canaux parallèles et à contre-courant. On montre que la matrice des coefficients A est de rang n - 1 et on donne la condition nécessaire et suffisante pour que A ait deux valeurs propres nulles.

### BEMERKUNGEN ZU EINIGEN EIGENSCHAFTEN VON WÄRMEÜBERGANGSGLEICHUNGEN FÜR VIELKANAL-WÄRMEÜBERTRAGER

**Zusammenfassung**—Einige Eigenschaften von Wärmeübergangsgleichungen für Vielkanal-Gleich- und Gegenstromwärmeübertrager werden diskutiert. Es wird gezeigt, dass die Matrix der Koeffizienten A vom Grad n - 1 ist und die für A notwendige und hinreichende Bedingung von zwei latenten Null-Wurzeln ist angegeben.

#### () НЕКОТОРЫХ СВОЙСТВАХ УРАВНЕНИЯ ПЕРЕНОСА ТЕПЛА В МНОГОКАНАЛЬНЫХ ТЕПЛООБМЕННИКАХ

Аннотация—Рассматриваются некоторые свойства уравнения переноса тепла в прямоточных и противоточных теплообменниках, состоящих из n каналов. Показано, что матрица коэффициентов A имеет ранг n-1. Приводится условие, необходимое и достаточное для того, чтобы коэффициенты A имели два нулевых характеристических корня.